### General Description

The MAX3667 is a complete, +3.3V laser driver with automatic power control (APC), designed for SDH/ SONET applications up to 622Mbps. It accepts differential PECL inputs, provides single-ended bias and modulation currents, and operates over a -40°C to +85°C temperature range.

A temperature-stabilized reference voltage simplifies laser current programming. It allows external programming of the modulation current between 5mAp-p and 60mAp-p, and of the bias current between 5mA and 90mA.

The APC function, which incorporates a monitor photodiode, an external resistor, and two external capacitors, maintains constant laser output power. Two current monitors provide high-speed signals that are directly proportional to the bias and modulation currents. Additional features include disable/enable control and a slow-start feature with a minimum turn-on time of 50ns. The MAX3667 is available in die form and in a 32-pin TQFP package.

### **Applications**

622Mbps SDH/SONET Access Nodes Laser Driver Transmitters Section Repeaters

### \_\_\_Features

- Single +3.3V or +5.0V Operation
- Automatic Average Power Control
- Bias Current and Modulation Current Monitor Outputs
- TTL-Compatible Disable Input
- Temperature-Compensated Reference
- PECL-Compatible Data Inputs

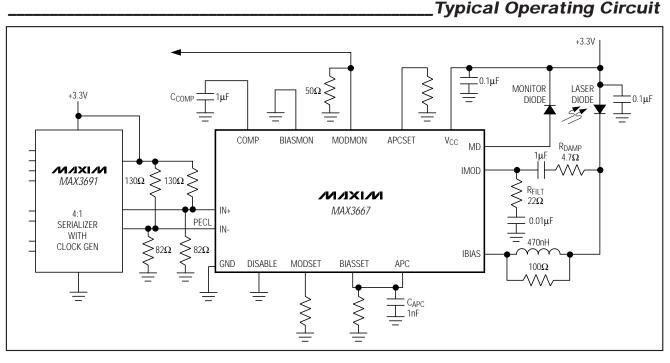
### Ordering Information

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PART	TEMP. RANGE	PIN-PACKAGE
MAX3667ECJ	-40°C to +85°C	32 TQFP
MAX3667E/D	-40°C to +85°C	Dice*

\*Dice are designed to operate from -40°C to +85°C but are tested and guaranteed only at  $T_j = +25$ °C.

Pin Configuration appears at end of data sheet.



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### **ABSOLUTE MAXIMUM RATINGS**

Supply Voltage, V <sub>CC</sub>	0.5V to +7.0V
Current into IBIAS	50mA to 350mA
Current into IMOD	50mA to 200mA
Current into MD	±7mA
Voltage at APC, MODMON,	
BIASMON, COMP	0.5V to (V <sub>CC</sub> + 0.5V)
Voltage at IN+, IN-, DISABLE, MODSET,	
BISASSET, APCSET, PULLUP	0.5V to (V <sub>CC</sub> + 0.5V)

Continuous Power Dissipation ( $T_A = +85^{\circ}C$ )	
TQFP (derate 11.1mW/°C above +85°C)721mW	
Operating Temperature Range40°C to +85°C	
Operating Junction Temperature Range (die)55°C to +175°C	
Processing Temperature (die)+400°C	
Storage Temperature Range65°C to +160°C	
Lead Temperature (soldering, 10sec)+300°C	

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### DC ELECTRICAL CHARACTERISTICS

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX
Supply Current (Note 3)	Icc	Closed loop (Note 4)		112	133
Bias Current Range	IBIAS	(Note 5)	5		90
Bias Off Current	IBIAS	Disable = high		5	250
Modulation Off Current	IBIAS	Disable = high		20	250
Internal Pull-Up Resistor (Note 6)	R <sub>PULL-UP</sub>		26	31	35
Reference Voltage (Note 7)	VREF	Disable = high or low	0.91	1.01	1.11
		$R_{BIASSET} = 2k\Omega$ , open loop (Note 8)		200	
Bias Current Stability		$R_{BIASSET} = 33.2 k \Omega$ , open loop (Note 8)		200	
		$R_{BIASSET} = 2k\Omega$ , closed loop (Notes 4, 9)			150
Modulation Current Stability		$R_{MODSET} = 2k\Omega$ , open loop (Note 8)		200	
Modulation Current Stability		$R_{MODSET} = 33.2 k\Omega$ , open loop (Note 8)		200	
BIASMON to IBIAS Gain	Al	$R_{BIASSET} = 2k\Omega$	30	38	46
MODMON to IQMOD Gain	AI	$R_{MODSET} = 2k\Omega$ (Note 13)	26	33	40
IBIASSET to IBIAS Gain	Aı	$R_{BIASSET} = 2k\Omega$	145	170	200
IRIASSEL IO IDIAS GUIL		$R_{BIASSET} = 33.2 k\Omega$	128	160	195
IMODSET to IQMOD Gain	Al	$R_{MODSET} = 2k\Omega$ (Note 13)	152	190	230
MODSEL 10 IOMOD Gain		$R_{MODSET} = 33.2 k\Omega$ (Note 13)	152	190	230
IAPCSET to IBIAS Gain	A	$R_{APCSET} = 2k\Omega$	135	170	205
APCSET TO IDIAS Gain	A	$R_{APCSET} = 33.2 k \Omega$	164	205	250
PECL Input High Voltage	VIH		2.14		
PECL Input Low Voltage	VIL				1.82
PECL Input High Current	IIН	V <sub>IN</sub> = 2.14V		4.5	10
PECL Input Low Current	IIН	V <sub>IN</sub> = 1.82V		2	10
TTL Disable High Voltage	VDIH		2.0		
TTL Disable Low Voltage	VDIL				0.8
TTL Disable High Current	IDIH			1	
TTL Disable Low Current	IDIL			4	



UNITS

mΑ

mΑ

μΑ

μΑ

Ω

V

ppm/°C

ppm/°C

A/A

A/A A/A

A/A

A/A

V

V

μA

μA

V

V

μA

μA

### DC ELECTRICAL CHARACTERISTICS

(V\_{CC} = +5.0V  $\pm$ 5%, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted.) (Notes 1, 2)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Supply Current (Note 3)	ICC	Closed loop (Note 4)		134	160	mA
Bias Off Current		Disable = high		2	250	μA
Modulation Off Current		Disable = high		32	250	μΑ
BIASMON to IBIAS Gain	AI	$R_{BIASSET} = 2k\mathbf{\Omega}$		38		A/A
MODMON to IQMOD Gain	AI	$R_{MODSET} = 2k\Omega$ (Note 13)	26	33	40	A/A
IBIASSET to IBIAS Gain	Δ.	$R_{BIASSET} = 2k\Omega$	145	180	220	A/A
	A	$R_{B ASSET} = 33.2k\mathbf{\Omega}$	143	180	215	
luce err to lou op Cain		$R_{MODSET} = 2k\Omega$ (Note 13)	168	240	315	A/A
I <sub>MODSET</sub> to IQMOD Gain	A	$R_{MODSET} = 33.2 k \Omega$ (Note 13)	188	230	285	
IAPCSET to IBIAS Gain	Δ.	$R_{APCSET} = 2k\Omega$	132	166	200	A/A
	A	$R_{APCSET} = 33.2 k \mathbf{\Omega}$	145	182	220	
PECL Input High Voltage	VIH		3.84			V
PECL Input Low Voltage	VIL				3.52	V
PECL Input High Current	Іін	V <sub>IN</sub> = 3.84V		9		μA
PECL Input Low Current	Іін	V <sub>IN</sub> = 3.52V		8		μA

### **AC ELECTRICAL CHARACTERISTICS**

 $(V_{CC} = +3.3V \pm 5\%, T_A = -40^{\circ}C$  to  $+85^{\circ}C, R_{LOAD} = 10\Omega$ , unless otherwise noted.) (Notes 2, 10)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Modulation Current Range	IMOD	$R_{FILT} = 22\Omega$ , $R_{DAMP} = 0\Omega$ (Note 11)	5		60	mA
Output Rise Time	+	V <sub>CC</sub> = 3.3V ±5%, 20% to 80%		270	450	- ps
	ι <sub>r</sub>	V <sub>CC</sub> = 5.0V ±5%, 20% to 80%		205	400	
Output Fall Time	tf	V <sub>CC</sub> = 3.3V ±5%, 20% to 80%		425	650	ps
	ır	V <sub>CC</sub> = 5.0V ±5%, 20% to 80%		315	600	
Output Aberrations				±10		%
Pulse-Width Distortion	PWD	$R_{FILT} = 22\Omega$ , $R_{DAMP} = 0\Omega$ (Note 12)		70		ps

**Note 1:** Dice are tested at  $T_A = +27^{\circ}C$ .

**Note 2:** Minimum voltage at IBIAS =  $V_{CC}$  - 1.6V.

**Note 3:** The sum of the currents flowing into V<sub>CC</sub> and PULLUP with R<sub>BIASSET</sub> = R<sub>MODSET</sub> = R<sub>APCSET</sub> =  $2k\Omega$ , IN+ = 1.82V, IN- = 2.14V.

Note 4: APC is connected to BIASSET for closed-loop operation.

**Note 5:** Bias current range is guaranteed by the I<sub>BIASSET</sub> to IBIAS gain test.

**Note 6:** R<sub>PULL-UP</sub> is connected between IMOD and PULLUP.

**Note 7:**  $V_{REF}$  is the voltage on BIASSET, MODSET, or APCSET with  $R_{BIASSET} = R_{MODSET} = R_{APCSET} = 2k\Omega$ .

**Note 8:** APC is disconnected from BIASSET for open-loop operation.

**Note 9:** Bias current stability is guaranteed by design and characterization.

**Note 10:** AC parameters are guaranteed by design and characterization.

**Note 11:** Modulation current range is guaranteed by the I<sub>MODSET</sub> to I<sub>OMOD</sub> gain test.

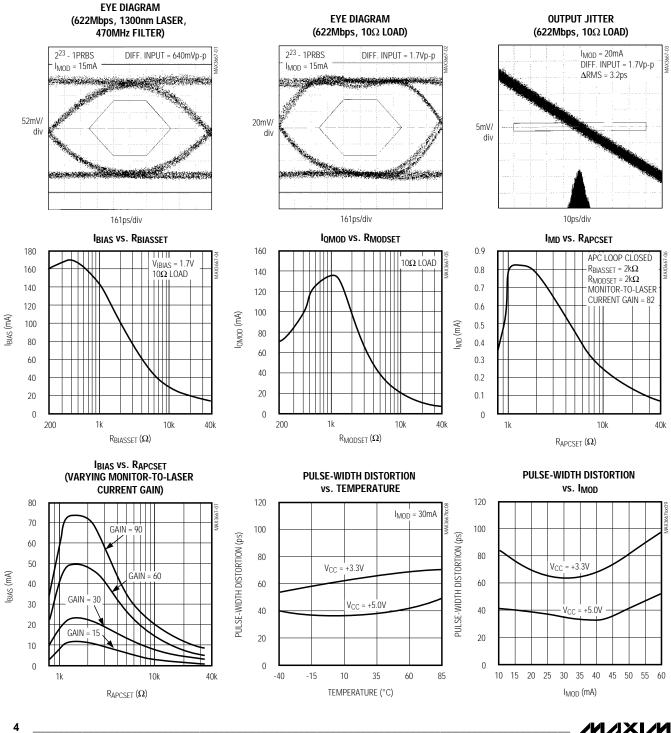
Note 12: Input signal is a 155Mbps 1-0 pattern. PWD = [(width of wider pulse) - (width of narrower pulse)] / 2.

Note 13:  $I_{QMOD}$  is the current flowing into the collector of  $Q_{MOD}$  (Figure 1).

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 $(T_A = +25^{\circ}C, V_{CC} = +3.3V, unless otherwise noted.)$ 

### **Typical Operating Characteristics**

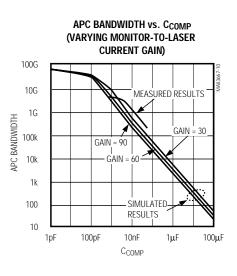


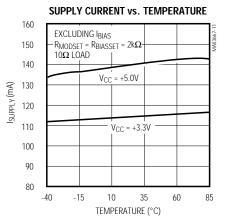
**MAX3667** 

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### \_Typical Operating Characteristics (continued)

 $(T_A = +25^{\circ}C, V_{CC} = +3.3V, unless otherwise noted.)$ 





### Pin Description

PIN	NAME	FUNCTION	
1, 2, 23, 24	V <sub>CC</sub>	Supply Voltage Input	
3, 6, 8, 13, 14, 15, 18, 20, 22	GND	Ground	
4	IN+	Positive PECL-Compatible Input	
5	IN-	Negative PECL-Compatible Input	
7	DISABLE	Disable Input. High = disable, TTL-compatible input.	
9, 26, 28, 31	N.C.	No Connection	
10	MODSET	Adjustment for Laser-Diode Modulation Current	
11	APC	Feedback Current for Closed-Loop Laser-Diode Bias Control	
12	BIASSET	Open-Loop Adjustment for Laser-Diode Bias Current	
16	IBIAS	Laser-Diode DC Bias Current	
17	PULLUP	$V_{CC}$ Supply for Internal 31 $\Omega$ Pull-Up Resistor	
19, 21	IMOD	Laser-Diode Modulation Current	
25	MD	Input for PIN Monitor Diode Current	
27	APCSET	Closed-Loop Adjustment for Laser-Diode Bias Current	
29	BIASMON	IBIAS Current Monitor (gain = 1/38 IBIAS). Open PNP collector, connect to ground if not used.	
30	MODMON	IMOD Current Monitor (gain = 1/33 IQMOD). Open PNP collector, connect to ground if not used.	
32	COMP	External Compensation Capacitor for Closed-Loop Laser-Diode Bias Current Control Stability	

### M/IXI/M

# **MAX3667**

### Detailed Description

Low-voltage operation of laser diodes and optical transmitters produces stringent headroom conditions for laser drivers. Fast changes in modulation current produce large inductive voltage spikes, creating device saturation problems. Therefore, for +3.3V operation, the MAX3667's modulation current should be AC coupled to the cathode of a laser diode. The recommended DC blocking capacitor value is  $1\mu$ F. A simplified block diagram of the modulation driver is shown in Figure 1.

The IMOD pin is internally biased through a  $31\Omega$  pull-up resistor. This design decouples the headroom associated with the modulation driver from the forward voltage drop of the laser diode, allowing the circuit to tolerate greater di/dt voltage transients. The design of the MAX3667 assumes a maximum DC forward-voltage drop of 1.6V across the laser diode. Bias current is DC coupled to the laser diode separately at the IBIAS output. In most applications, some small amount of resistance should be added in series with the DC blocking capacitor to help damp out the aberrations created by parasitic elements.

### **Automatic Power Control**

The automatic power control (APC) feature allows an optical transmitter to maintain constant power, despite changes in laser efficiency due to temperature and aging. The APC loop requires the use of a PIN monitor photodiode, which generates a current proportional to the laser diode output power. A scaled version of the current flowing into the MD pin is compared to a scaled version of the current flowing out of the APCSET pin. When these currents are of equal value, the inputs of the operational transconductance amplifier (OTA) are balanced, and COMP is forced to approximately 1V.

When the average value of the monitor diode current exceeds the value established by the APCSET current, the COMP voltage is forced lower. If the average value of the monitor diode current is less than the value established by the APCSET current, the COMP node voltage is forced higher. The output of the OTA (the APC pin), when connected directly to BIASSET (closed-loop condition), is used as an error signal to adjust the bias current flowing into BIASSET. The maximum OTA output current is approximately ±250µA.

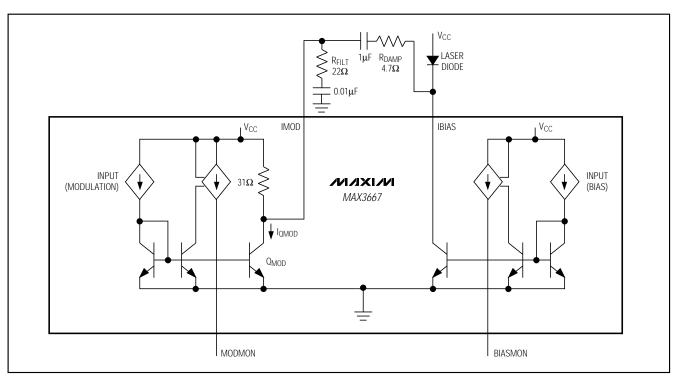


Figure 1. Simplified Modulation Driver Block Diagram

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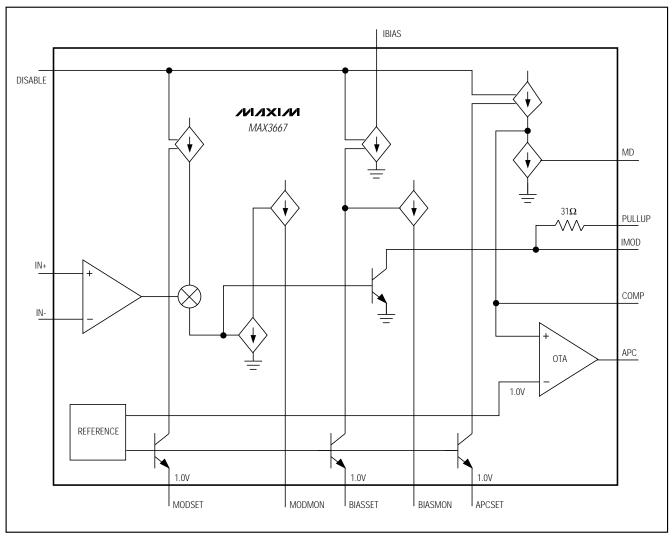


Figure 2. Block Diagram

Closed-loop operation requires the user to establish three internal currents with external resistors placed between ground and the BIASSET, MODSET, and APC-SET pins. See the *Design Procedures* section for guidelines on selecting these resistor values.

### **Open-Loop Operation**

If desired, the MAX3667 is fully operational without the use of the APC loop. In these types of applications, the laser diode current is set solely by the external resistors connected to the BIASSET and MODSET pins. See the *Design Procedures* section for instructions on setting up the MAX3667 for open-loop operation.

#### **Disable Control**

The MAX3667 provides a single-ended TTL-compatible disable control pin. The IBIAS, IMOD, and APCSET currents are disabled when the voltage on this pin is set high. However, the internal voltage reference and other sections of the MAX3667 remain active to ensure predictable operation and faster enable response times. The disable response time is approximately 25ns.

### **Temperature Considerations**

The MAX3667 contains a voltage reference that is fully temperature compensated. This reference is used throughout the circuit, as well as for programming the



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bias, modulation, and monitor diode current levels. Where necessary, the reference is adjusted by a VBE voltage to cancel thermal errors created by the BIASSET, MODSET, and APCSET current mirrors. This ensures that the IBIAS and IMOD currents are nearly constant over temperature with open-loop operation. With the APC loop closed, this reference helps maintain a constant average MD current (and thus a constant average laser output power) over temperature.

**Bias and Modulation Current Monitors** 

The BIASMON and MODMON analog output monitors provide current levels that are directly proportional to the IBIAS and IMOD currents levels. These currents can be used in conjunction with other external circuitry to supervise the performance of the laser driver system without adding parasitics or reducing system performance. The gains associated with these pins, relative to IBIAS and IQMOD, are approximately 1/38 (for BIASMON) and approximately 1/33 (for MODMON).

In addition to a scaled copy of the modulation current, the MODMON current contains a DC offset current used internally to keep the driver transistors functioning at high speed, even with low modulation levels. This current is not precisely controlled and should be ignored when using the MODMON feature.

### Design Procedure

### **Programming the Modulation Current**

In addition to being a function of RMODSET, IMOD is also dependent on the values of the series damping resistor ( $R_{DAMP}$ ), the shunt compensation resistance ( $R_{FILT}$ ), and the resistance of the laser diode (Figure 1).

If  $I_{QMOD}$  represents the total current flowing into the collector of  $Q_{MOD}$ , then the modulation current into the laser diode can be represented by the following:

$$I_{MOD} = I_{QMOD} \begin{bmatrix} 31\Omega \mid |R_{FILT} \\ \hline 31\Omega \mid |R_{FILT} + (R_{DAMP} + r_{LASER}) \end{bmatrix}$$
$$I_{QMOD} = (A_I)(I_{MODSET})$$
$$A_I = I_{MODSET} \text{ to } I_{MOD} \text{ Gain}$$

Assuming RFILT =  $22\Omega$ , RDAMP =  $4.7\Omega$ , and rLASER =  $4\Omega$ , then this equation is simplified to:

$$I_{MOD} = I_{QMOD}(0.6)$$

For R<sub>DAMP</sub> =  $4.7\Omega$ , R<sub>FILT</sub> =  $22\Omega$ , and a laser resistance of approximately  $4\Omega$ , refer to the I<sub>QMOD</sub> Current vs. R<sub>MODSET</sub> graph in the *Typical Operating Characteristics* and select the value of R<sub>MODSET</sub> that corresponds to the required current at +25°C.

### Programming the Bias Current (open loop)

When operating the MAX3667 without APC, program the bias-current output by adjusting the BIASSET resistor. To select this resistor, determine the desired bias current required at +25°C. Refer to the IBIAS Current vs. RBIASSET graph in the *Typical Operating Characteristics*, and select the value of RBIASSET that corresponds to the required current.

### Programming the Automatic Power Control (APC)

When using the MAX3667's APC feature, program the bias-current output by adjusting the APCSET resistor. To select this resistor, determine the desired monitor current to be maintained over temperature. Refer to the MD Current vs. RAPCSET graph in the *Typical Operating Characteristics*, and select the value of RAPCSET that corresponds to the required current.

When using the APC feature, be sure to connect the APC pin directly to BIASSET (see the *Typical Operating Circuit*). In this mode, the bias-current output level is no longer controlled by the BIASSET resistor. The APCSET resistor is now controlling the output bias level. Under closed-loop conditions, RBIASSET assures that the feedback current range is properly centered. It is recommended that RBIASSET be chosen to equal RAPCSET during closed-loop operation.

### **Pattern-Dependent Jitter**

To reduce pattern-dependent-jitter (PDJ) effects, two external compensation capacitors are required to ensure that the control loop responds slowly to changes in laser efficiency. The overall time constant of the APC loop is set by the value of these capacitors, by the transfer ratio between the laser diode current and the monitor diode current, and by the MAX3667's openloop gain.

C<sub>COMP</sub> must be placed between the COMP pin and ground; C<sub>APC</sub> must be placed between the APC pin and ground (see the *Typical Operating Circuit*). For 622Mbps SDH/SONET applications, the recommended values of C<sub>COMP</sub> and C<sub>APC</sub> are 1µF and 1nF, respectively.



Since the PDJ will change with changes in loop gain, it is important to choose capacitor values that are as large as is physically possible. Since each capacitor represents a different pole, for stability reasons, CAPC should be kept substantially smaller than C<sub>COMP</sub>. It is recommended that the value of C<sub>APC</sub> be set 1000 times smaller than C<sub>COMP</sub>.

The time constant associated with the DC blocking capacitor on IMOD can also have an effect on PDJ. It is important that this time constant produce minimum droop for long consecutive bit streams.

Referring to Figure 3, the droop resulting from long time periods without transitions can be represented by the following equation:

$$[100\% - \mathsf{DROOP}] = \mathrm{e}^{\frac{-\mathrm{t}}{\tau}}$$

APC operation assures that the discharge level for  $\tau$  is PAVG. An overall droop of 6% relative to P<sub>p-p</sub> equates to a 12% droop relative to PAVG. To ensure a droop of less than 12% (6% relative to P<sub>p-p</sub>), this equation can be solved for  $\tau$  as follows:

$$\tau = \frac{-t}{\ln[1 - 0.12]} = 7.8t$$

If  $t_1$  equals 100 consecutive unit intervals without a transition, then the time constant associated with the DC blocking capacitor needs to be longer than:

 $\tau_{AC} \geq R_{AC}C_{AC} = 7.8 \text{ (100 bits) (1.6ns/bit)} = 1.25 \mu s$  The estimated value of R<sub>AC</sub> is:

 $R_{AC} = 31\Omega \parallel R_{FILT} \parallel (R_{DAMP} + r_{LASER})$ 

Assuming R<sub>FILT</sub> = 22 $\Omega$ , R<sub>DAMP</sub> = 4.7 $\Omega$ , and r<sub>LASER</sub> = 4 $\Omega$ , R<sub>AC</sub> = 5.2 $\Omega$ 

with  $C_{AC} = 1\mu F$ ,  $\tau_{AC} = 5.2\mu s$ .

#### **Operation without APC (open loop)**

When operating without APC, be sure to configure the MAX3667 as follows:

- 1) Disconnect APC from BIASSET.
- 2) Force a voltage of 1V to 2V at APC to prevent the OTA from saturating.
- 3) Disconnect the monitor diode.
- 4) Pull up the MD pin to V<sub>CC</sub> through a  $5k\Omega$  resistor.
- 5) Pull down the COMP pin to ground through a  $30k\Omega$  resistor.

Remember that the bias-current output is programmed by adjusting the BIASSET resistor when the APC loop is disconnected.

Figure 3. Droop

### **Output Current Limits**

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The MAX3667 is equipped with output current limiting and short-circuit protection. In +3.3V operation, IBIAS is limited to approximately 170mA open loop, and IQMOD is limited to approximately 140mA (see *Typical Operating Characteristics*). In +5.0V operation, IBIAS is limited to approximately 300mA, and IQMOD is limited to approximately 140mA.

If BIASSET is shorted to ground, IBIAS becomes current limited. If either APCSET or MODSET is shorted to ground, the MAX3667 output is turned off. Note that in +5.0V operation, the IBIAS current limit is approximately 300mA. Care should be taken if the MAX3667 is being used with a laser diode that is sensitive to this current level.

### Interface Suggestions and Laser Compensation

Adding damping resistance in series with the laser diode (typically  $3\Omega$  to  $5\Omega$ ) raises the load resistance, reduces the load frequency dependence and improves output aberrations. A series damping resistor of 4.7 $\Omega$  is suggested for the MAX3667.

Series inductance at the cathode of the laser results in high-frequency loading (V<sub>L</sub> = Ldi/dt) and increased output aberrations. Because of reduced headroom, the output performance of the transmitted eye diagram can be significantly impacted during +3.3V operation. Assuming that laser package series inductance can not be completely eliminated, a compensation network is required. With a laser diode load of approximately 4 $\Omega$  and 4nH, a series damping resistor of 4.7 $\Omega$ , and a coupling capacitor of 0.1µF, a shunt R-C compensation network of 22 $\Omega$  and 0.01µF is recommended (see Typical Operating Circuit). These values may need to be adjusted depending on the style of laser used. Note that it is important to place the compensation network as close to the load as possible.

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**MAX3667** 

Since the IBIAS output is also connected directly to the laser cathode, any parasitic capacitance associated with this output must not be allowed to significantly load the response. To resolve this problem, place an R-L compensation network in series with the IBIAS output. The additional high-frequency impedance of this network will help maintain a high impedance at this node. The recommended values for this resistance and inductance are 100 $\Omega$  and 470nH, respectively.

Optimize the laser diode performance by placing a bypass capacitor as close to the anode pin as possible. Use good high-frequency layout techniques and multilayer boards with uninterrupted ground planes.

### **Input Termination Requirements**

The MAX3667 data inputs are PECL compatible. Standard PECL levels require  $50\Omega$  terminations to V<sub>CC</sub> - 2V. The MAX3667's common-mode input range is 1.5V to (V<sub>CC</sub> - 0.75V) with a minimum differential input swing of 620mVp-p. The MAX3667's inputs need not be driven with standard PECL signals; as long as the common-mode voltage and differential swing is met, the device will operate properly.  $50\Omega$  input termination is also not required, but is recommended for good high-frequency termination.

#### Wire Bonding

For high current density and reliable operation, the MAX3667 uses gold metalization. Make connections to the die with gold wire only, using ball-bonding techniques. Wedge bonding is not recommended. Die-pad size is 4 mils (100mm) square, and die thickness is 12 mils (300µm).

### \_Applications Information

### DC-Coupled Operation and Output Current Limits

To improve headroom conditions for the MAX3667, AC coupling of the modulation current is required at +3.3V operation. At +5.0V operation, AC coupling is suggested but not required.

For AC-coupled operation, the total output current is equal to IBIAS + IMOD / 2. For DC-coupled modulation currents, the total output current is equal to IBIAS + IMOD.

#### Optimizing Performance for Low Modulation Currents

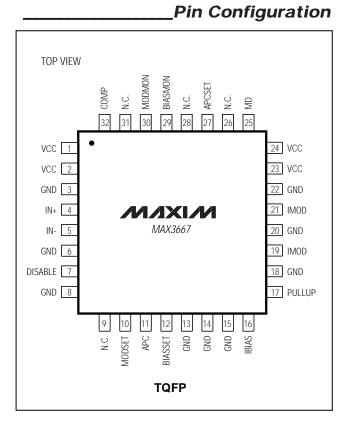
The MAX3667's dynamic range and headroom requirements are such that, in order to meet these specifications, low-current performance is compromised. If continual operation at low modulation currents ( $\leq$  20mA) is the intended application, the MAX3667's high-frequency performance can be improved with an external pull-up resistor. By shunting the AC current away form the laser diode, this technique reduces the output swing without reducing the operating current of the output transistor. Maintaining a higher modulation operating current level preserves the high-frequency performance of the output device. A suggested starting point for the external pull-up resistor value is 100 $\Omega$ .

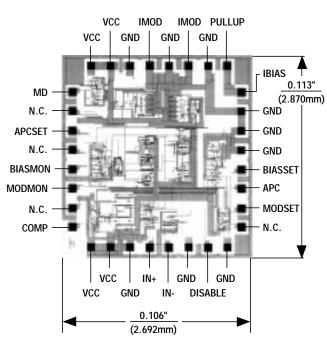
### Modulation Currents Greater than 60mA

At +5.0V operation, the headroom conditions for the MAX3667 are improved significantly. In this mode, it is possible to achieve modulation currents greater than 60mA by floating PULLUP and driving the laser diode directly (DC-coupled IMOD).

#### Laser Safety and IEC 825

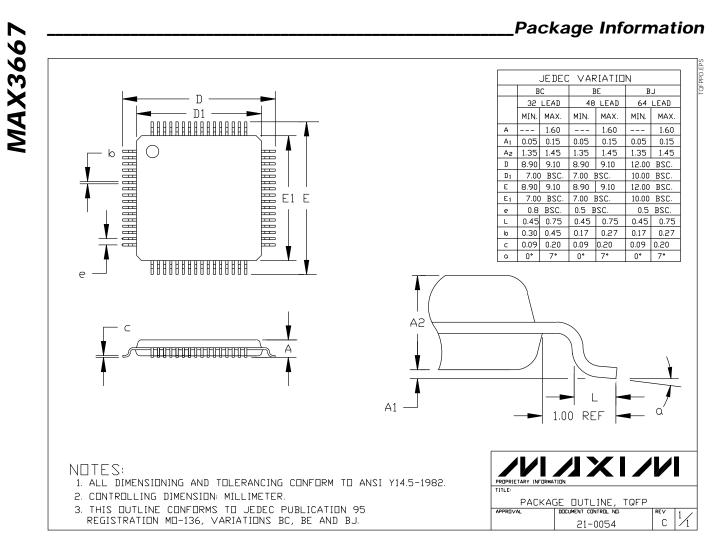
Using the MAX3667 laser driver alone does not ensure that a transmitter design is compliant with IEC 825. The entire transmitter circuit and component selections must be considered. Each customer must determine the level of fault tolerance required by their application, recognizing that Maxim products are not designed or authorized for use as components in systems intended for surgical implant into the body, for applications intended to support or sustain life, or for any other application where the failure of a Maxim product could create a situation where personal injury or death may occur.





### Chip Topography

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